1 Evidence for an Explosive Origin of Central Pit Craters on Mars

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5 Abstract:

Kilometer-scale pit craters are nested in the centers of many impact craters on Mars as 6 7 well as on icy satellites. They have been inferred to form in the presence of a water-ice rich 8 substrate; however, the process(es) responsible for their formation is still debated. Leading 9 models invoke origins by either explosive excavation, or by subsurface drainage and collapse. If explosive excavation forms central pits, ejecta blankets should be draped around the pits, 10 whereas internal collapse should not deposit significant material outside pit rims. Using visible 11 12 wavelength images from the MRO CTX and HiRISE instruments and thermal infrared images from the Odyssey THEMIS instrument, we conducted a survey to characterize, in detail, the 13 global population of central pits in impact craters ≥ 10 km in diameter. We specifically examined 14 15 the morphology and thermophysical characteristics of the pits for evidence of pit ejecta. Our analysis of thermal images suggests that coarse-grained materials - which we interpret as pit 16 17 ejecta – are distributed proximally around many central pits on the floors of their parent craters. These observations and interpretations support an explosive origin for central pits on Mars. We 18 19 present an alternative "uplift contact model" to explain the formation of central pits late in the 20 impact process. Theoretical calculations show that more than enough thermal energy is available 21 via impact melt from the parent crater to form central pits by steam explosions, and such explosions would require only a modest amount (2-6% by volume) of uplifted water-ice. We 22

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therefore propose that central pits on Mars could have formed explosively by the interaction ofimpact melt and subsurface water-ice.

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26 Introduction:

Nested central pit craters on Mars have remained enigmatic structures for several 27 decades. Their formation is typically believed to be connected with subsurface water due to their 28 29 relative abundance on Mars and icy satellites, but the exact role of water and the specific process(es) responsible for forming central pits are still debated. In this study, we make thermal 30 inertia observations of central pit craters to test hypotheses for central pit formation. We start 31 with an overview of the previously proposed hypotheses and the gaps in our understanding. 32 Then, we discuss the utility of thermal inertia in remotely determining grain size distributions 33 34 around central pits. We hypothesize that central pits are formed by explosive excavation or 35 devolatilization during or after impact. After analyzing our results, we present an alternative model for central pit formation that -- uniquely among other pit origin hypotheses -- creates an 36 37 explosion late enough in the impact process for central pits to be preserved. Finally, we apply our integrated observations to interpret the morphology and thermal properties of central pits in the 38 context of central uplifts and propose testable predictions for the model. 39

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41 Background:

Central pits occur in many impact structures on Mars and exhibit a crater-in-crater configuration [*e.g.*: Smith, 1976; Hodges, 1978; Barlow *et al.*, 2000; Barlow, 2010] (Fig. 1). Kilometer-scale central pits have been identified on the floors or on top of the central peaks of over 1,000 Martian impact craters with diameters as large as 125 km in diameter and down to as

small as 5 km in diameter [Smith, 1976; Barlow and Bradley, 1990; Barlow *et al.*, 2000; Barlow, 2011]. In our study, we focus on "floor pits" that are deeper than the surrounding floor of their parent craters, as opposed to "summit pits" that occur atop the central peaks. Based an ongoing survey by Barlow [2010, 2011] and this study, central floor pits have a median diameter of 0.16-0.175 parent crater radii, such that a 50 km diameter crater might have a central pit ~8 km wide. Their depths range from very shallow to over 1.5 km below the surrounding impact crater floor.

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Fig. 1: THEMIS daytime IR mosaic of a 50 km diameter unnamed Martian impact crater
 containing a central pit at 296.4°E, 17.6°S. A MOLA topographic profile across the center shows
 typical pit morphology.

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Central pit craters on Mars are confined to low and mid-latitudes, within ±70° of the Martian equator [Hodges *et al.*, 1980; Barlow, 2011; Garner and Barlow, 2012]. Central pits are also common for impact craters on icy satellites, including Ganymede and Callisto [Smith *et al.*, 1979]. Central pits are seldom observed on rocky planets other than Mars, although a few dozen are present on Mercury [Schultz, 1988; Xiao and Komatsu, 2013] and the Moon [Croft, 1981; Schultz, 1976a, 1976b, 1988; Xiao *et al.*, 2014].

64 The presence of water-ice is believed to be involved in typical pit formation [Hodges et al., 1980; Croft, 1981]. Although water-ice is not stable on low-latitude Martian surfaces today 65 [Clifford and Hillel, 1983; Mellon *et al.*, 1997; Head *et al.*, 2003], water was (and might still be) 66 67 present within the upper few kilometers of the surface even at low latitudes earlier in Mars' history. The possibility of significant subsurface water in pre-impact terrains is supported by the 68 presence of layered ejecta surrounding many fresh Martian impact craters [Carr et al., 1977; 69 70 Gault and Greeley, 1978; Wohletz and Sheridan, 1983; Barlow et al., 2000; Baloga et al., 2005] 71 and Mars Odyssey Gamma Ray Spectrometer spectra [Boynton et al., 2007]. However, the process(es) responsible for forming central pits in impact craters and the role of water are still 72 debated, and several mechanisms for pit formation have previously been proposed. 73

Wood *et al.* [1978] proposed explosive decompression may volatilize a subsurface waterrich layer, causing steam explosions and removing the core of central peaks. However, this model suffers from the difficulty of keeping water vapor from escaping early in the impact process before a central pit can be preserved [Croft, 1981; Pierazzo *et al.*, 2005; Senft and Stewart, 2011; Elder *et al.*, 2012].

Croft [1981], Bray [2009], Senft and Stewart [2011], Alzate and Barlow [2011] and Elder *et al.* [2012] proposed central pits could form by the melting then gravitational drainage of target water-ice through fractures underlying central uplifts. However, raised rims are also associated with many Martian central pits [Wood *et al.*, 1978; Garner and Barlow, 2012] and would not be expected with collapse structures. These models also require large volumes of water to be drained, which is unrealistic for forming the central pits on the Moon and Mercury.

Passey and Shoemaker [1982], Bray *et al.* [2012], and Greeley *et al.* [1982] proposed central peaks of impacts in weak target materials may collapse to form central pits. However, the

abundance of impact craters with central peaks and summit pits in the same regions as impact
craters with floor pits suggests the target material should be strong enough to prevent collapse
[Barlow, 2011].

Greeley *et al.* [1982] proposed and demonstrated in laboratory experiments that smallscale central pits can be excavated from impacts into layered targets causing central peak detachment. Schultz [1988] also proposed central pits are excavated as a primary result of impacts with low-velocity bolides. However, scaling up to planetary impact craters with diameters of tens of kilometers is problematic because the material-strength crater is larger than the gravity-controlled transient crater, greatly reducing the influence of any strength differences on the final crater morphology [Croft, 1981].

For this study, we group the previously proposed mechanisms for pit formation into those 97 98 that explosively remove material upward and outward [e.g.: Wood et al., 1978; Greeley et al., 99 1982; Schultz, 1988] and those that remove material downward [e.g.: Croft, 1981; Passey and 100 Shoemaker, 1982]. During a crater-forming explosion, rocks and boulders are ejected out of the 101 crater, layers are proximally uplifted and overturned, and ejecta is draped over the surrounding surface to create raised rims [e.g. Melosh, 1989]. The average grain size for ejecta decreases with 102 radial distance from the crater, such that the largest clasts or blocks are proximal to the crater rim 103 104 [e.g.: Gault et al., 1963; O'Keefe and Ahrens, 1985; Melosh, 1989; Buhl, 2014]. Features such as 105 sinkholes, which are typical of karst landscapes, and lava tube skylights form by gravitational collapse and do not create raised rims nor emplace material atop their rims [e.g., Okubo and 106 107 Martel, 1998; Salvati and Sasowsky, 2002; Cushing et al., 2007; Robinson et al., 2012]. The presence or absence of an ejecta blanket around central pits provides one way to distinguish 108

109 between explosive versus collapse scenarios for the formation of central pits. A property of

110 ejecta blankets is decreasing average grain size with distance from an explosively-derived crater.

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112 Data and Methods:

For this study, we surveyed and identified impact craters > -10 km in diameter 113 containing central floor pits within $\pm 60^{\circ}$ latitude of the Martian equator using the Java-based 114 115 planetary geographic information system program JMARS [Christensen et al., 2009]. Central pits were identified as distinctive circular depressions in the center of an impact crater that 116 appeared to be deeper than the parent crater floor based on the available imaging and 117 topography. Many small impact craters with diameters <10 km containing central depressions 118 were excluded from our survey due to poor spatial resolution, as well as craters we could not 119 120 confidently determine had depressions deeper than the parent floor. We excluded summit pits 121 that occur atop central peaks and are not deeper than the parent crater floor to avoid potential bias from coherent rock or boulders on the sides of the central peaks. We also excluded 122 123 ambiguous structures that might be peak rings or concentric terraces, especially in craters near the Martian simple to complex crater transition of ~6-7 km diameter [Garvin et al., 2000, 2003]. 124

Diameters were measured for both the central pits and their parent craters. Most central pits were too small to identify in the 128 pixel/deg (460 m/px) Mars Orbiter Laser Altimeter (MOLA) global mosaic [Smith *et al.*, 2001], so the ~100 m/pixel Mars Odyssey mission Thermal Emission Imaging Spectrometer (THEMIS) [Christensen *et al.*, 2004] calibrated daytime infrared (IR) global mosaic [Edwards *et al.*, 2011] was used instead, which provides nearly complete coverage to $\pm 60^{\circ}$ latitude. THEMIS daytime IR images show topography as shaded relief, since sun-facing slopes are typically warmest. Higher resolution visible images were also used to

132 observe finer-scale morphology and distinguish central morphologies that appeared ambiguous 133 in THEMIS daytime IR. Primarily, we used Mars Reconnaissance Orbiter mission Context Camera (CTX) [Malin et al., 2007; Bell et al., 2013] images at ~ 6 m/pixel that were map-134 135 projected and photometrically stretched from Planetary Data System (PDS) raw electronic data records, and where available we used High Resolution Imaging Science Experiment (HiRISE) 136 [McEwen et al., 2007] images at ~ 0.25 to 1.3 m/pixel that were map-projected and 137 138 photometrically stretched from PDS calibrated reduced data records. The global dust environment for central pit crater context is shown using Thermal Emission Spectrometer (TES) 139 solar energy reflectivity (albedo) integrated from 0.3 to 2.9 µm [Christensen et al., 2001]. 140

During the formation of impact and other explosive craters, coarse debris are typically 141 ejected and scattered outside the crater. Large blocks and coarse grains have a higher thermal 142 143 inertia than finer-grained materials and hold on to their heat longer through the night. This 144 thermal inertia can be calculated from nighttime thermal images and used to estimate average grain size [Christensen, 1986]. We therefore used the THEMIS thermal inertia global mosaic as a 145 146 quantitative proxy for average grain size, such that coarse-grained or blocky materials have relatively higher thermal inertias (warmer at night) while dust, sand, and other fine-grained 147 materials have lower thermal inertias (cooler at night) [Christensen, 1986; Fergason et al., 2006; 148 149 Edwards et al., 2009; Edwards et al., 2011]. THEMIS nighttime images and thermal inertias 150 have previously been used to identify blocky ejecta rays from impact craters on Mars that otherwise show little or no albedo variation in visible images but where grain size trends are seen 151 with respect to distance from the crater [McEwen et al., 2005; Tornabene et al., 2006]. Central 152 pits with an annulus or a geographically skewed patch of higher thermal inertia material nearer 153

154 the pit rim than more distally across the surrounding parent crater floor may be classified as 155 having a fining average grain size with radial distance, consistent with ejecta.

To measure the trend of thermal inertias, we circumferentially averaged the THEMIS 156 157 thermal inertia mosaic over central pit craters in intervals of 0.1 parent crater radii. Because most 158 central pits are <0.2 crater radii, we compare pit-proximal averaged thermal inertia values within the interval from 0.2-0.3 crater radii versus more distal averaged thermal inertia values at 0.5-0.6 159 160 crater radii. A Student's t-test is then performed on the differences between proximal and distal 161 averaged thermal inertias for the population of central pits. A significance level of $P \ge 0.05$ would be deemed not statistically significant and serves as our null hypothesis: thermal inertia and 162 average grain size do not decrease radially away from pit rims. For P<0.05, a radial decrease in 163 thermal inertia with distance from the pit rim would be deemed statistically significant and we 164 165 would reject the null hypothesis and support an alternative hypothesis that ejecta surrounds central pits. 166

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168 **Results:**

We identified central floor pits within 654 parent craters ~10 km diameter or larger 169 between $\pm 60^{\circ}$ latitude of the Martian equator (Fig. 2). Additional smaller craters with central pits 170 171 exist [Barlow, 2010, 2011], but are not well-resolved in the THEMIS thermal images used for this study. MOLA topographic profiles have very coarse resolution and may only provide insight 172 to the largest central pit craters (Fig. 1), although complete and partially rimmed pits frequently 173 occur in the highlands terrains [Garner and Barlow, 2012]. We identified central pits in parent 174 impact craters with diameters ranging from ~8 to 114 km, with 95% of those parent craters being 175 176 <50 km in diameter and excluding smaller potential central pit craters. The surveyed central pits

- have a median diameter ratio to their parent craters of 0.175 with a standard deviation of 0.037
- 178 (Fig. 3). These results are comparable to the median ratio of 0.16 found by Barlow [2011].
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Fig. 3: Histogram showing the range of diameter ratios between central pits and their parent craters that we measured. The median value is 0.175 with a standard deviation of 0.037.

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191 Based on THEMIS-derived thermal inertias, most central pits showed higher thermal inertia (coarser) material near their rim than more distally on the parent crater floor (e.g. Fig. 4). 192 193 635 of the 654 central pits had thermal images over their parent crater floors, of which 395 194 (62%) had higher average proximal thermal inertias outside the pits (between 0.2-0.3 crater radii) 195 than more distally (between 0.5-0.6 crater radii), and 240 (38%) had the same or lower thermal inertia proximally than distally. Notably, 76% (254 out of 333) of central pits with diameters >20 196 km have radially decreasing thermal inertia trends, 80% (175 out of 216) of central pits with 197 198 near-pit thermal inertia values >300 TIU (less dusty) have radially decreasing thermal inertia 199 trends, and 89% (74 out of 83) of central pits satisfying both of the above selection criteria have 200 radially decreasing thermal inertia trends. Pits with proximal high and radially decreasing 201 thermal inertias in THEMIS images sometimes show large blocky debris (up to tens of meters

- 202 wide) in visible CTX and HiRISE images (Fig. 5), while pits that did not show proximally high
- 203 nor decreasing thermal inertias typically appeared blanketed or mantled (Fig. 6).



Fig. 4: THEMIS nighttime (color) and CTX visible (shading) images showing radially decreasing high thermal inertia material interpreted as ejecta surrounding two central pit craters at A) 18.4°S, 102.7°E, and B) 14.9°S, 93.2°E. Color scales indicate thermal inertia values.



Fig. 5: A) HiRISE image showing large blocks near a central pit crater at 23.8°S, 126.8°E. B)

211 THEMIS nighttime IR (color) over daytime IR (shading) context image showing high-thermal

212 inertia material inferred as being blocky and confirmed by the HiRISE image. Black lines

213 indicate location of A. Yellow box in B indicates footprint of HiRISE image.

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Fig. 6: A) THEMIS nighttime IR (color) over CTX visible (shading) image showing a central pit
crater at 10.9°N, 50.8°E without a radially decreasing thermal inertia. Average thermal inertia
values are uniformly low across the crater floor and associated with a coating of fine-grained
dust. B) HiRISE visible image enlargement of an area near the central pit showing low-contrast
dust mantling the terrain.

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We conducted a paired Student's t-test to determine the confidence interval of the measured thermal inertia decreases from 0.2-0.3 crater radii to 0.5-0.6 crater radii. For the 635 central pit craters with thermal images, the t-test returns a P<0.01 indicating extreme statistical significance. We therefore reject our null hypothesis that thermal inertia and average grain size do not decrease radially away from pit rims, and support an alternative hypothesis that pits are surrounded by ejecta with grain size decreasing with distance away from the pit.

229 Central pits in Tharsis, Elysium, Arabia, and other dusty regions, characterized by high 230 TES albedos and low thermal inertia values, tend to not be surrounded by material with radially 231 decreasing thermal inertia trends (Fig. 1). The median proximal thermal inertia for central pits

with radially decreasing thermal inertias is 283 thermal inertia units (1 $TIU = 1 \text{ J m}^{-2}\text{K}^{-1}\text{s}^{-1/2}$) with a standard deviation of 121 TIU, while the median proximal thermal inertia for central pits with other, radially non-decreasing thermal inertia trends is 205 TIU with a standard deviation of 145 TIU (Fig. 7).



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Fig. 7: Histogram and box-and-whisker plot of central pit craters exhibiting radially decreasing thermal inertia trends (red) and radially non-decreasing thermal inertia trends (blue) plotted against THEMIS thermal inertia values. Lower thermal inertias are indicative of finer average grain size and dustiness.

Smaller central pits also tend not to show radially decreasing thermal inertias (Fig. 8). Based on the population of impact craters observed with THEMIS data, the median diameter for parent craters containing pits with warm material is ~23.3 km and the median diameter for craters with pits lacking it is ~16.7 km, both cases being above the simple/complex transition of 6-7 km for Martian craters [Garvin *et al.*, 2000, 2003].



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Fig. 8: Histogram and box-and-whisker plot of craters containing central pits exhibiting radially
 decreasing thermal inertia trends (red) and radially non-decreasing thermal inertia trends (blue)
 plotted against parent crater diameter.

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254 **Discussion:**

255 The raised rims around some pits [Wood, 1978; Garner and Barlow, 2012] are suggestive of explosive excavation, similar to their parent craters, which also have raised rims. As discussed 256 257 by Garner and Barlow [2012], raised rims are more frequently observed in larger central pits than smaller ones. They also argue that the preferred distribution of rimmed pits in highlands regions 258 and non-rimmed pits in volcanic plains suggests that target material strength and/or volatile 259 content may also limit the expression of raised rims. Some very small scale pits on Mars 260 believed to have formed from volatile release in impact melt have been identified and also 261 exhibit slightly raised rims, although they are not exclusive to crater centers and do not exhibit 262 well-defined ejecta blankets [Tornabene et al., 2012; Boyce et al., 2012]. Surfaces visible in 263 some CTX and HiRISE images show large (meter-scale) blocks in warm patches adjacent to 264 265 central pits (e.g., Fig. 5), consistent with the expected correlation between warm material and coarse surfaces. Such blocks and megablocks are commonly observed near explosively-formed 266 craters, including at the Ries crater in Germany [e.g. Gault et al., 1963], as well as at some 267 268 Martian craters [e.g., Caudill et al., 2012]. Combined with the spatial correlation of warm material and central pits, we interpret the blocks scattered around central pits to be explosively-269 emplaced pit ejecta. 270

The observability of high thermal inertia, coarse-grained material appears linked to the size of the pit. Small craters excavate smaller volumes of material that is finer-grained on average than larger craters [*e.g.*: Gault *et al.*, 1963; O'Keefe and Ahrens, 1985; Melosh, 1989; Buhl, 2014]. Fine-grained rocks are more easily eroded or buried than coarser-grained rocks, so the coarser ejecta at larger pits should be preferentially preserved and less buried. Surface diurnal thermal inertias are sensitive to materials within a few thermal skin depths (several centimeters)

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of the surface, so any ejecta would have to be buried by no more than a few centimeters of dust

in order to be observable. Accumulated dust and sand is frequently observed on Mars and is indicated in our analysis as low thermal inertia values due to dust's fine grain size (Fig. 6). The smaller grain size distribution of ejecta for smaller craters is therefore expected to decrease the positive detection of ejecta using diurnal thermal inertias.

The presence of high thermal inertia material on parent crater floors near pits would not 282 necessarily need to be due to ejecta. To avoid many false-positives, we have calculated the trend 283 284 in thermal inertia (grain size) with radial distance from the pit. For example, post-impact lava or perhaps impact melt flows occur on the floors of some craters containing central and have high 285 thermal inertias, although small flow lobes are easily distinguishable (Fig. 9), and more extensive 286 lava or impact melt flows could potentially fill central pits. We expect impact melt ponds to be 287 288 distributed throughout the crater floor, so measuring a radially decreasing trend in thermal inertia 289 as opposed to only using high thermal inertia values avoids this problem in most cases. Patchy or 290 partial erosional uncovering of consolidated parent crater fill rocks could also explain higher 291 thermal inertias relative to the surrounding crater floor; however, we consider the selective removal of significant amounts of dust from the centers of parent craters, but not in the dusty 292 plains surrounding many parent craters, to be unlikely. Additionally, significant erosion on the 293 294 parent crater floor is inconsistent with the presence and preservation of raised rims around many central pits. Thermal inertias are also low for relatively fine-grained aeolian dunes or other 295 bedforms that often form in the centers of craters, and confirmed in CTX and HiRISE images 296 (Fig. 6). 297



Fig. 9: THEMIS nighttime IR (color) over CTX visible (shading) image showing high thermal inertia lava flow lobes (red, oranges, and yellow irregular bands on crater floor) on the floor of

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inertia lava flow lobes (red, oranges, and yellow irregular bands on crater floor) on the floor of an impact crater containing a central pit at 28.5°N, 83.4°E.

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303 The results of our thermal inertia study are consistent with and support both the Wood *et* 304 al. [1978] and Greeley et al. [1982] models; however, each suffers from a critical weakness. The Wood *et al.* [1978] model for an explosive pit origin suffers from the difficulty of keeping vapor 305 from escaping early in the impact process before a pit can be preserved. The Greeley et al. 306 307 [1982] central peak detachment model also suffers from issues scaling up from the laboratory to 308 planetary impact craters. Alternatively, an explosive reaction could potentially result from 309 mixing of water-ice and molten rock through several mechanisms. For example, a post-impact 310 magmatic intrusion could intrude into a crater and react with the ground water as a maar volcano 311 [Wohletz, 1986; Begét et al., 1996]; however, we would not expect such a scenario to consistently form pits in crater centers. Heavy fracturing and brecciation during the impact 312

313 process may allow fluids (either impact melt, or liquid water) to mobilize and permeate the 314 substrate and come into contact with each other, similar to the fluid flow described by Elder et al. [2012]. Although liquid water may move freely through fractures, Elder et al. finds that 315 316 impact melt would cool too quickly due to its high melting temperature and larger temperature 317 difference with the country rock. Rain or ice-bearing fallback ejecta could also be deposited on top of impact melt pools or suevite deposits [Segura et al., 2002], but that would not necessarily 318 319 require that pits always form in the centers of their parent craters, nor that they be consistently sized. Below, we describe an alternate model for bringing water into contact with impact melt. 320

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322 Alternate Pit Formation Model:

We present an alternate hypothesis that -- unique among other pit origin hypotheses --323 324 predicts an explosion late enough in the impact process for central pits to be preserved and has a properly scaled analog. In our uplift contact model, impact central uplifts bring water (as liquid, 325 ice, or both) vertically up and into contact with near-surface impact melt to initiate late-stage 326 327 steam explosions and form central pits (Fig. 10). Central uplift occurs late in the impact process during the modification stage, after most crater fill has settled [e.g., Melosh, 1989]; thus, pit 328 formation concurrent with central uplift is consistent with the apparent lack of infilling of deep 329 pits. As we describe in the next paragraph, our explosive central pit model is akin to an inverted 330 maar volcano [e.g. White and Ross, 2011], except instead of magma rising up into contact with 331 332 groundwater or permafrost, a water-bearing substrate is uplifted into contact with impact melt. 333 Similarly-scaled events have been observed at monogenetic maar volcanoes with diameters of up to 8 km on the Seward Peninsula in Alaska [Begét et al., 1996], where the permafrost buffers the 334 335 water-magma interaction to achieve high heat transfer efficiencies [Wohletz, 1986].



Fig. 10: Schematic cartoons illustrating steps in complex crater formation resulting in: A) a
 classical central peak [modified from French, 1998], and B) our proposed new "uplift contact
 model" for Martian central pit crater formation.

As the central uplift rises, it brings deeply-sourced water-bearing rock from below the 342 transient cavity up into contact with shallow crater fill deposits and impact melts. We would not 343 expect significant vertical mixing of sub-transient cavity material outside the central uplift, so 344 these large pits should always be in the centers of their parent impact craters. As the water-345 bearing central uplift rises into contact with impact melt and other hot debris, the thermal energy 346 from the melt may be transferred to the water, resulting in a steam explosion to eject material 347 outward, raise rims, and deposit ejecta surrounding the pits (with average grain sizes decreasing 348 with radial distance, as we found in this study). As material is ejected outwards, the walls may 349 become unstable and slump hot debris and impact melt into the pit cavity. There, the new rush of 350

351 melt and hot rocks may again react with uplifting water to recharge the system and iteratively 352 trigger a series of explosions to further deepen and widen the central pit. When central uplift 353 slows, the vertical mixing of water decreases and the explosions will cease.

We explored the theoretical plausibility of whether enough thermal energy could have been available in a post-impact environment to initiate steam explosions capable of creating kilometer-scale central pits. We started with the empirical model shown below which predicts the mass ratio of melted (m_m) to displaced (m_d) impact target materials in a silicate target (Eq. 1) [O'Keefe and Ahrens, 1982; Melosh, 1989]:

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$$m_m/m_d = 1.6 \times 10^{-7} \times (g \times D_i)^{0.83} \times v_i^{0.33}$$
 (1),

where *g* is planetary gravity, D_i is parent crater diameter and v_i is bolide velocity. We assign the following values for our calculations: gravity $g = 3.711 \text{ m/s}^2$ and bolide velocity $v_i = 10 \text{ km/s}$ [Ivanov *et al.*, 2002]. We also assumed that any melt generated remained within the parent crater. Finally, we modeled the parent crater as a half-ellipsoid and applied the mass fraction to determine the volume and mass of melt produced (Eqs. 2,3):

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$$V_m = (m_m/m_d) \times (2/3) \times \pi \times d_i \times (D_i/2)^2$$
 (2) and

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$$m_m = \rho_m / V_m$$
 (3),

where V_m is the volume of melt, d_i is the depth of the parent crater, and ρ_m is the density of the melt. We assume a depth of complex craters (in km) of $d_i = 0.357 D_i^{0.52}$ [Tornabene *et al.*, 2013]. Sato and Taniguchi [1997] used the following empirical equation to predict the energy required to form a crater via volcanic, nuclear, and chemical explosions, independent of origin. The equation can similarly be applied to central pits (Eq. 4):

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$$E_c = 4.45 \times 10^6 \times D_p^{-3.05}$$
 (4),

where E_c is the energy of pit formation and D_p is the diameter of the pit, for which we assume a median pit-to-parent crater diameter ratio of 0.16 [Barlow, 2010, 2011]. The total thermal energy transfer required to melt ice and boil water to steam can be calculated using specific and latent heats (Eq. 5):

$$H_w = m_w \times L_f + m_w \times c_{lq} \times \Delta T_w + m_w \times L_v \quad (5),$$

where H_w is the energy transferred to the water, m_w is the mass of water, L_f is the latent heat of 378 fusion, c_{lq} is the specific heat of liquid water, ΔT_w is the temperature change of liquid water, and 379 L_v is the latent heat of vaporization. We assign values for $L_f = 3.34 \times 10^5$ J/kg, $c_{lq} = 4.187 \times 10^3$ 380 J/kg·K, and $L_v = 2.257 \text{ x}10^6 \text{ J/kg}$ [Moran and Shapiro, 2008]. Evaluating Eq. 5, we see that an 381 investment of 3.023x10⁶ J is required to turn 1 kg of water from ice (273 K) to steam (373 K). 382 We assume that the steam is not heated to higher temperatures, although a smaller amount of 383 384 superheated steam might also satisfy the energy requirements for explosivity. The thermal 385 energy of vaporization, specifically the step of converting water to steam, can be transformed to kinetic energy that can form a pit. The mass of steam required is calculated by dividing the pit 386 387 formation energy from Eq. 4 by the latent heat of vaporization. Dividing this result by the density of ice provides the volume of ice required to form a central pit. As shown in Fig. 11, assuming a 388 half-ellipsoidal pit geometry with the pit depth (in km) $d_p = 0.276 D_p^{0.68}$ [Tornabene *et al.*, 2013], 389 only a small amount of water (comprising 2-6% of a central pit's volume) would need to be 390 vaporized to form a central pit for the parent crater diameters observed (5-125 km [Barlow, 391 392 2011]).



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Fig. 11: Required amounts of water and impact melt for heat energy transfer to form a kilometerscale (pit) crater shown as percent by volume with respect to the volume of a central pit crater.
The range in impact melt volume represents uncertainty due to varying heat transfer efficiency
between 0.1-0.3.

399 The amount of thermal energy available in impact melt may also be calculated using 400 specific heats (Eq. 6):

(6),

$$E_m = m_m \times c_{pm} \times \Delta T_m = \rho_m \times V_m \times c_{pm} \times \Delta T_m$$

where E_m is the energy required for cooling rock, c_{pm} is the specific heat of rock, ΔT_m is the temperature change of the rock. We assume a basaltic melt composition and assign values of ρ_m = 2900 kg/m³ [Judd and Shakoor, 1989]; c_{pm} = 1000 J/kg·K [Wohletz, 1986]; and change of temperature (from the basalt solidus to the STP boiling point of water) $\Delta T_m = 1473$ K – 373 K =

406 1100 K [Wohletz, 1986]. It should be noted that impact melts can also be superheated, perhaps up to 1700°C (1973 K) [Zieg and Marsh, 2005], so our calculations may underestimate the 407 thermal energy available by \sim 50%. Adiabatic heat transfer efficiency is typically \sim 0.1 or less due 408 409 to poor mixing; however, it can reach an optimal efficiency of ~ 0.3 for water/melt ratios of 0.3-410 0.5 [Wohletz, 1986]. Such optimal efficiencies are believed to be present for maars in permafrost, as suggested by the largest, kilometer-scale terrestrial maars found in the Seward 411 412 Peninsula, Alaska [Begét et al., 1996]. Our calculations consider cases with both 0.1 413 (suboptimal) and 0.3 (optimal) efficiencies.

The mass of impact melt required to vaporize ice to steam can be calculated by setting the 414 total heat transfer H_w from Eq. 5 equal to the product of the heat transfer efficiency and the 415 impact melt thermal energy from Eq. 6. As shown in Fig. 11, the impact melt must comprise a 416 417 volume greater than or equal to 6-18% of the central pit's volume for an optimal thermal 418 efficiency of 0.3, or 17-55% of the central pit's volume for a suboptimal thermal efficiency of 419 0.1. The total energy transfer required for vaporizing ice (H_w) from Eq. 5 can also be compared 420 to the total energy available from impact melt by multiplying Eq. 6 with the value(s) for heat transfer efficiency (Figs. 12,13). Based on these calculations, sufficient thermal energy should be 421 available via impact melt to vaporize small amounts of ice that act explosively to form central 422 pits within kilometer-scale impact structures. However, not all Martian craters exhibit central 423 pits. Below, we discuss the material requirements may inhibit the explosive formation of some 424 425 central pits on Mars.







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Fig. 13: Ratios of available / required thermal energy for vaporizing enough steam to explode
and form a central pit, with respect to crater diameter. The range of in energy ratios reflects
variations in heat transfer efficiency over a range of 0.1 (lower curve) to 0.3 (upper curve).

First, an appropriate volume of water must be available in the central uplift. If too little 437 438 water (or too low a concentration) is present, there may not be sufficient steam to form a large pit. Even if water was initially present in the target rocks, large impacts (with crater diameters of 439 several tens to hundreds of km) likely remove most subsurface volatiles early in the impact 440 process such that not enough water is available to react with the impact melt to form a pit. 441 Conversely, if the system has excess water, there may not be enough thermal energy in the 442 443 impact melt to heat the excess water and still vaporize enough to sustain an explosion and make 444 a pit.

445 Second, an appropriate volume of impact melt must be retained within the parent impact crater. Smaller impact craters produce less melt proportionally and distribute that impact melt 446 more sparsely, so small craters may not have enough consolidated impact melt even if enough 447 448 water is present. Larger impact craters might also produce excess impact melt that could fill in 449 any central pits that might form. A similar phenomenon is thought to have occurred at the Sudbury impact structure, where steam explosions created the brecciated Onaping Formation but 450 451 the explosive depressions themselves were filled in and erased [Grieve et al., 2010]. Another 452 interesting aspect of the uplift contact model is that since our calculations show it only requires small amounts of water (perhaps as little as 2-6% by volume), it provides a possible explanation 453 for the formation of the small number of central pits observed on Mercury [Schultz, 1988; Xiao 454 and Komatsu, 2013] and the Moon [Croft, 1981; Schultz, 1976a, 1976b, 1988; Xiao et al., 2014], 455 456 which should have insufficient water or other volatiles to form by drainage and collapse models 457 [e.g. Croft, 1981]. Although we did not measure summit pit-related thermal inertias in our survey, summit pits would be expected to form as in our uplift contact model when steam 458 459 explosions start but become water- or impact melt-limited. In such a case, the explosive reaction fails before uplift has ceased and an incomplete pit is left superposed on a remnant central peak. 460

Based on our uplift contact model, we propose the following testable predictions. First, a the ejecta deposit is expected to contain abundant fractured and fragmented glassy impact melt, similar to the Onaping Formation at Sudbury [Grieve *et al.*, 2010]. This layer of glassy deposits should overlay more coherent impact melt deposits. Second, lithic clasts and mineral assemblages found stratigraphically below the transient crater should be found on the floor of the parent crater, with the greatest abundance proximal to the rim. Third, the stratigraphic sequence

of rocks around central pits should be overturned. Finally, *in situ* measurements of material
around the pit should show decreasing average grain sizes with radial distance from central pits.

470 Conclusions:

The presence of raised rims and blocky material surrounding Martian central pits are 471 suggestive of ejecta from an explosive pit origin. Over 60% of all central pits in our global 472 473 survey have material with radially decreasing thermal inertias around them, and 89% of central pits craters with diameters >20 km and non-dusty proximal thermal inertias >300 TIU have 474 radially decreasing thermal inertias. The population of central pit craters as a whole has a 475 statistically significant (P<0.01) decrease in thermal inertia radially outwards from pit rims. We 476 interpret these findings as a typical decrease in average grain size with increasing distance away 477 478 from central pits. As expected, dust masks the diurnal thermal signature around many central 479 pits. This effect is amplified in smaller pits due to their less voluminous and finer-grained ejecta 480 that are more easily buried or eroded. Previously proposed models do not satisfactorily explain 481 all observed characteristics of central pits. We have therefore proposed a new "uplift contact model" to explain the observed morphologies (i.e., geometries, raised rims) and thermal 482 properties (radially decreasing thermal inertias/average grain size) of Martian central pit craters. 483 484 Our thermal calculations show that only \geq 2-6% water by volume is required to create a phreatomagmatic explosion and form central pits. Our explosive origin model is also 485 advantageous over drainage and collapse models in explaining the small number of central pits 486 on Mercury and the Moon using only minor amounts of volatiles in localized pre-impact 487 subsurfaces. Drainage and collapse may still be a viable method for pit formation on icy 488

489	satellites, but an explosive origin appears to be the preferred mechanism on Mars (and other
490	rocky planets) for forming central pit craters.
491	
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